

A unified shallow water/Dupuit-Forchheimer approach to solve large scale Aquifer flows.

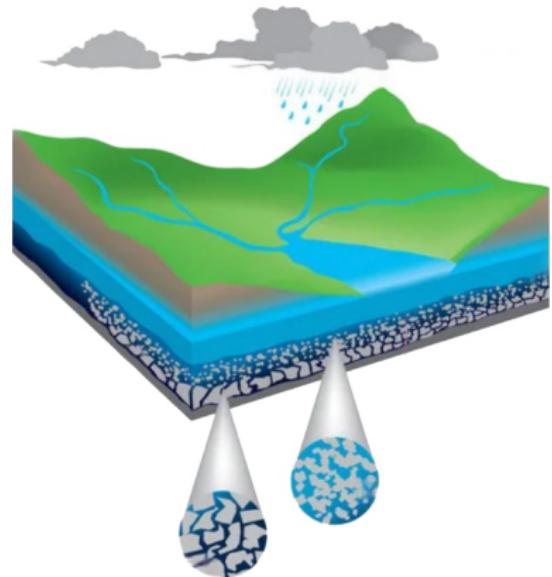
45ème Congrès National d'Analyse Numérique

Manon CARREAU Martin PARISOT

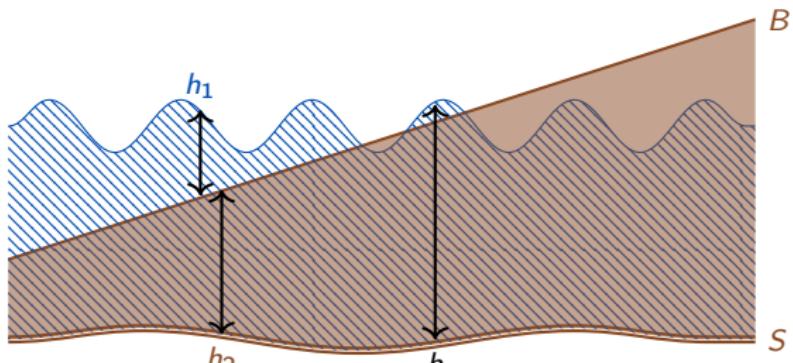
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- ▶ free flow surface on a porous media ;
- ▶ large aquifer ;
- ▶ long time simulations ;
 - flooding,
 - sand beach,
 - water infiltration,
- ▶ more complicated topology ;
 - multi-layers free surface/porous media,
 - congestion, roof and floating body,
 - confined aquifer.



$$\begin{cases} \partial_t V + \nabla \cdot (\mathcal{V}_1 \bar{u} - \bar{\kappa} \mathcal{V}_2 \nabla \phi) = 0 \\ \partial_t (\mathcal{V}_1 \bar{u}) + \nabla \cdot (\mathcal{V}_1 \bar{u} \otimes \bar{u}) = -\mathcal{V}_1 \nabla \phi - \frac{\bar{u}}{2} (G)_+ \\ G = -(\partial_t \mathcal{V}_1 + \nabla \cdot (\mathcal{V}_1 \bar{u})) \end{cases}$$



The unknowns :

- ▶ ϕ , the potential ;
- ▶ \bar{u} , horizontal velocity.

Secondary variables :

- | | |
|---|---|
| <ul style="list-style-type: none"> ▶ $h = \phi/g - S$; ▶ $h_2 = \min(h, B - S)$; ▶ $h_1 = h - h_2$. ▶ κ hydraulic conductivity | <ul style="list-style-type: none"> ▶ $\mathcal{V}_1 = \bar{s}_1 h_1$; ▶ $\mathcal{V}_2 = \bar{s}_2 h_2$; ▶ $V = \mathcal{V}_1 + \mathcal{V}_2$. ▶ $\bar{V} = \bar{s}_2 (B - S)$ |
|---|---|

Initial data : $h(0, x) = h_0(x)$ and $\bar{u}(0, x) = u_0(x)$.

$$\epsilon \ll 1$$

(E)

(SW₂)

$$\bar{\kappa} \ll 1$$

(SW/DF)

- ▶ Can also be integrate from the Navier-Stokes model ;
- ▶ **mono-valuated** free-surface ;
 - η the water table and \bar{s} the space that the water can occupied

- ▶ $V_1(t, x) = \int_{B(x)}^{\infty} s(t, x, z) dz$ and $V_2(t, x) = \int_{S(x)}^{B(x)} s(t, x, z) dz$,
- ▶ $\bar{u}_1(t, x) = \frac{1}{V_1} \int_B^{\infty} su dz$ and $\bar{u}_2(t, x) = \frac{1}{V_2} \int_S^B su dz$,
- ▶ uniform horizontal velocity ;

$$\partial_t s + \nabla \cdot (su) + \partial_z(sw) = 0$$

$$s(\partial_t u + u \cdot \nabla u + w \partial_z u) = s \left(-\frac{\nabla p}{\rho} - \frac{u}{\kappa} \right)$$

$$s(\partial_t w + u \cdot \nabla w + w \partial_z w) = s \left(-\frac{\partial_z p}{\rho} - \frac{w}{\kappa} - g \right).$$

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(E)

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$$\begin{array}{|c|} \hline \partial_t s + \nabla \cdot (su) + \partial_z (sw) = 0 \\ \hline \end{array} \quad \downarrow \quad \begin{array}{|c|} \hline \partial_t V_1 + \nabla \cdot (V_1 \bar{u}_1) = -G \\ \hline \end{array}$$

$$\begin{array}{|c|} \hline \partial_t V_2 + \nabla \cdot (V_2 \bar{u}_2) = G \\ \hline \end{array}$$

$\epsilon \ll 1$

(E)

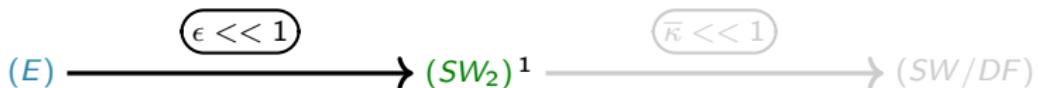
 $\bar{\kappa} \ll 1$ (SW₂)

(SW/DF)

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- ▶ **mono-valuated** free-surface ;
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- ▶ uniform horizontal velocity ;
- ▶ **hydrostatic** pressure ;
 - $p = \rho g (\eta - z) + O(\varepsilon^2)$,
- ▶ uniform hydraulic conductivity.

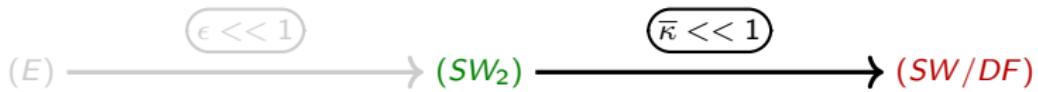
$$\begin{aligned} s(\partial_t u + u \cdot \nabla u + w \partial_z u) &= s \left(-\frac{\nabla p}{\rho} - \frac{u}{\kappa} \right) \\ s(\partial_t w + u \cdot \nabla w + w \partial_z w) &= s \left(-\frac{\partial_z p}{\rho} - \frac{w}{\kappa} - g \right). \end{aligned}$$

$$\begin{aligned} \partial_t (V_1 \bar{u}_1) + \nabla \cdot (V_1 \bar{u}_1 \otimes \bar{u}_1) &= -g V_1 \nabla (h + S) - \frac{V_1 \bar{u}_1}{\bar{\kappa}_1} - u_B G \\ \partial_t (V_2 \bar{u}_2) + \nabla \cdot (V_2 \bar{u}_2 \otimes \bar{u}_2) &= -g V_2 \nabla (h + S) - \frac{V_2 \bar{u}_2}{\bar{\kappa}_2} + u_B G \end{aligned}$$



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$$\begin{aligned} \partial_t V_1 + \nabla \cdot (V_1 \bar{u}_1) &= -G \\ \partial_t V_2 + \nabla \cdot (V_2 \bar{u}_2) &= G \\ \partial_t (V_1 \bar{u}_1) + \nabla \cdot (V_1 \bar{u}_1 \otimes \bar{u}_1) &= -g V_1 \nabla (h + S) - \frac{V_1 \bar{u}_1}{\bar{\kappa}_1} - u_B G \\ \partial_t (V_2 \bar{u}_2) + \nabla \cdot (V_2 \bar{u}_2 \otimes \bar{u}_2) &= -g V_2 \nabla (h + S) - \frac{V_2 \bar{u}_2}{\bar{\kappa}_2} + u_B G \end{aligned}$$



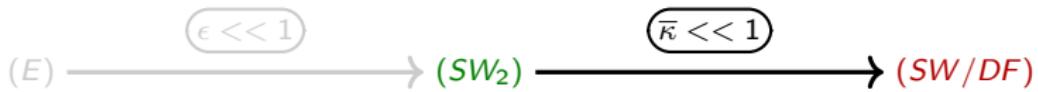
- ▶ $\bar{s}(x, z) = \begin{cases} \bar{s}_1(x) & \text{if } B \leq z, \\ \bar{s}_2(x) & \text{if } S \leq z < B. \end{cases}$
- ▶ $\bar{\kappa}_1(x) = \infty$ and $\bar{\kappa}_2(x) = O(K_2)$
- ▶ $V_2 = \sum_{i=0}^{\infty} K_2^i V_2^{(i)}, \quad \bar{u}_2 = \sum_{i=0}^{\infty} K_2^i \bar{u}_2^{(i)} \quad \text{and} \quad G = \sum_{i=0}^{\infty} K_2^i G^{(i)}$

Main Order

$$\boxed{\kappa_2 \left(\partial_t \left(V_2^{(0)} \bar{u}_2^{(0)} \right) + \nabla \cdot \left(V_2^{(0)} \bar{u}_2^{(0)} \otimes \bar{u}_2^{(0)} \right) \right) = -g \kappa_2 V_2^{(0)} \nabla \left(h^{(0)} + S \right) - V_2^{(0)} \bar{u}_2^{(0)} + \kappa_2 u_B^{(0)} G^{(0)}}$$

↓

$\bar{u}_2^{(0)} = 0$



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Second Order

The diagram illustrates the second-order derivation process. It starts with two equations enclosed in dashed boxes:

$$0 = -g V_2^{(0)} \nabla (h^{(0)} + S) - \frac{V_2^{(0)} \bar{u}_2^{(1)}}{\bar{\kappa}_2^{(1)}} + u_B^{(0)} G^{(0)}$$

$$\partial_t V_2^{(0)} = G^{(0)}$$

Arrows point from these equations to a central result:

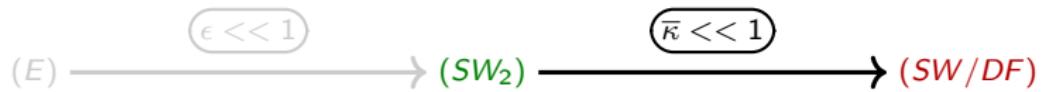
$$V_2 \bar{u}_2 = -g \bar{\kappa}_2 V_2 \nabla (h + S) + O(K_2)$$

Below this, another arrow points to a result in a red box:

$$G^{(0)} = 0$$

To the left, a circle contains the equation:

$$\bar{\kappa}_2^{(1)} = \frac{K_2}{\bar{\kappa}_2}$$



- ▶ $\bar{s}(x, z) = \begin{cases} \bar{s}_1(x) & \text{if } B \leq z, \\ \bar{s}_2(x) & \text{if } S \leq z < B. \end{cases}$
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$$\partial_t V + \nabla \cdot (V_1 \bar{u} - \bar{\kappa} V_2 \nabla \phi) = 0$$

$$\partial_t (V_1 \bar{u}) + \nabla \cdot (V_1 \bar{u} \otimes \bar{u}) = -V_1 \nabla \phi - \frac{\bar{u}}{2} (G)_+$$

$$G = -(\partial_t V_1 + \nabla \cdot (V_1 \bar{u}))$$

Energy dissipation law

$$\partial_t(\mathcal{E} + V_1 \frac{|\bar{u}_1|^2}{2}) + \nabla(\phi(V_1 \bar{u}_1 - \bar{\kappa}_2 V_2 \nabla \phi) + V_1 \bar{u}_1 \frac{|\bar{u}_1|^2}{2}) \leq -\kappa_2 V_2 |\nabla \phi|^2$$

- ▶ stability of the model

CPR scheme²

- ▶ IMEX-scheme
- ▶ stable & consistent
- ▶ asymptotic preserving

2. Edwige Godlewski et al. "Congested shallow water model: on floating body". In : [SMAI Journal of Computational Mathematics \(2021\)](#). doi : 10.5802/smai-jcm.67. url : <https://hal.inria.fr/hal-01871708>.

Energy dissipation law

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CFL

$$\frac{\delta_t}{\delta_x} \sum_{f \in \mathbb{F}_k} (F_{1,f} \cdot N_k^{k_f})^- < \frac{V_{1,k}^{SW}}{2}.$$

- ▶ $F_{1,f}$ the shallow water flux at the interfaces
- ▶ δ_t time step
- ▶ $V_{1,k}^{SW}$ shallow water volume explicitly calculate with only shallow water flux
- ▶ $N_k^{k_f}$ normal from the face k to k_f
- ▶ δ_x space interval

Energy dissipation law

$$\partial_t(\mathcal{E} + V_1 \frac{|\bar{u}_1|^2}{2}) + \nabla(\phi(V_1 \bar{u}_1 - \bar{\kappa}_2 V_2 \nabla \phi) + V_1 \bar{u}_1 \frac{|\bar{u}_1|^2}{2}) \leq -\bar{\kappa}_2 V_2 |\nabla \phi|^2$$

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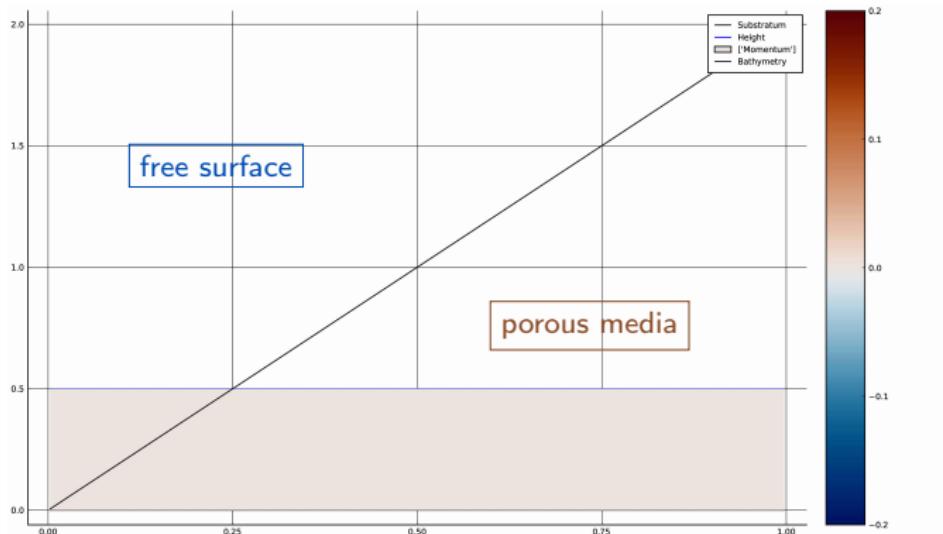
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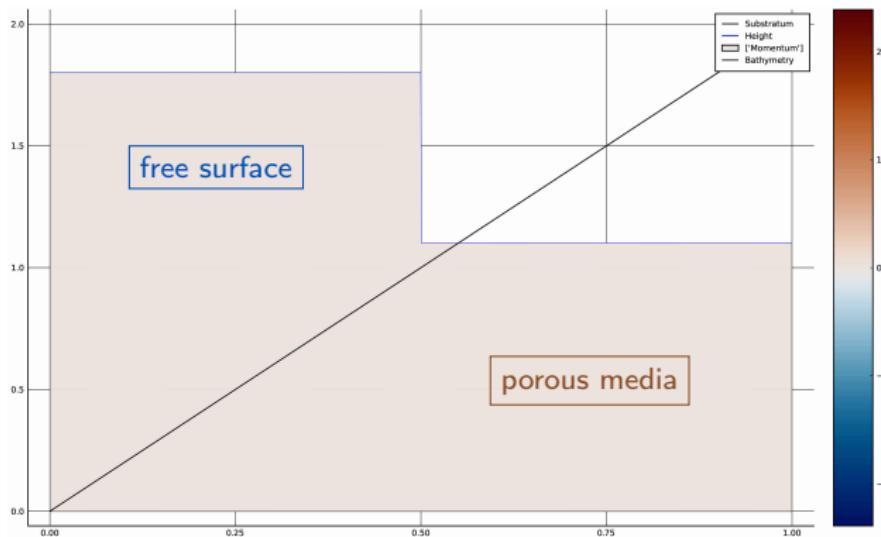
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- ▶ δ_t time step
- ▶ $N_k^{k_f}$ normal from the face k to k_f
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- ▶ $V_{1,k}^{SW}$ shallow water volume explicitly calculate with only shallow water flux
-  when $V_{1,k}^{SW} \rightarrow 0$



- ▶ $B(x) = 2x$
- ▶ $T^{max} = 5000$
- ▶ $h(1, t) = 1.2 + 0.3 \frac{\cos(\pi t)}{5000/2}$
- ▶ $S(x) = 0$
- ▶ $\delta_x = 5.10^{-3}$
- ▶ $h(0, t)$: wall
- ▶ $h_0(x) = 0.5$
- ▶ $s_2 = 0.5$
- ▶ restriction on δ_t



- ▶ $B(x) = 2x$
- ▶ $S(x) = 0$
- ▶ $h_0(x) = \begin{cases} 1.8 & \text{if } x < 0.5 \\ 1.1 & \end{cases}$
- ▶ $T^{max} = 5000$
- ▶ $\delta_x = 5.10^{-3}$
- ▶ $s_2 = 0.8$
- ▶ $\gamma_{CPR} = 10$
- ▶ $h(0, t)$: wall
- ▶ $h(1, t)$: wall
- ▶ restriction on δ_t

Video Links

- ▶ take an experiment
- ▶ choose a phenomenon to highlight
- ▶ check the behavior of the scheme

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End of the thesis objectives :

- ▶ roof
- ▶ non-permeable part in the porous media
- ▶ free surface part in the porous media
- ▶ thin free surface flow on the porous media

Youtube source : https://www.youtube.com/watch?v=bgEWf_ps5xs

- Audusse, Emmanuel et al. "A multilayer Saint-Venant system with mass exchanges for shallow water flows. Derivation and numerical validation". In : ESAIM: M2AN 45.1 (2011), p. 169-200.
doi : 10.1051/m2an/2010036. url : <https://doi.org/10.1051/m2an/2010036>.
- Godlewski, Edwige et al. "Congested shallow water model: on floating body". In : SMAI Journal of Computational Mathematics (2021). doi : 10.5802/smai-jcm.67. url : <https://hal.inria.fr/hal-01871708>.