Un schéma volume fini en une étape, tout régime, équilibré et entropique pour la dynamique des gas avec gravité.

Rémi Bourgeois*, Pascal Tremblin, Samuel Kokh CEA-Saclay, Maison de la simulation



CANUM 2020+2 Évian les Bains Minisymposium Lagrange Projection





Summary

- **convection**?
- Numerical results
- Why does it works ? -Flux splitting approach-

*Chalons et al. 2016 An all-regime Lagrange-Projection like scheme for the gas dynamics equations on unstructured meshes

Why do we need all-regime well-balanced numerical methods to study

The new solver as a algorithmic simplification of an existing method*

Star's structure: the convective zone



Thermally driven hydrodynamical convection



Physical problem: Condition for the convection instability in star's atmospheres

convective motion start after we apply a perturbation ?

Two approaches to compare and cross validate:

-Analytical: Using the linear stability analysis of Tremblin et al. 2019

-> Encapsulates most known convective instabilities and predicts new ones, -> *Easy* to extend to additional physics (MHD).

-Numerical: Via finite volume simulation using a stable well-balanced, all-regime method

-> Allows to conserve the conservative quantities up to machine precision. -> Good behavior at low speed, at the beginning of the instability (all-regime), -> Does not generate numerical perturbation around the initial equilibrium (well-balanced),

Under which conditions on the vertical profiles (temperature, pressure etc..) will the

Physical problem: Condition for the convection instability in star's atmospheres. Importance of the well-balanced property



Physical problem: Condition for the convection instability in star's atmospheres. Importance of the well-balanced property



- convection ?
- Numerical results
- Why does it works ? -Flux splitting approach-•

*Chalons et al. 2016 An all-regime Lagrange-Projection like scheme for the gas dynamics equations on unstructured meshes



Why do we need all-regime well-balanced numerical methods to study

The new solver as a algorithmic simplification of an existing method*

All Regime and/or Well balanced methods -some previous works-

- -J. M. Greenberg et al. Analysis and approximation of conservation laws with source terms.
- -L. Gosse. A well-balanced flux-vector splitting scheme designed for hyperbolic systems of conservation laws with source terms.
- -F. Bouchut. Nonlinear stability of finite volume methods for hyperbolic conservation laws and well-balanced schemes for sources.
- -P. Chandrashekar et al. A second order well-balanced finite volume scheme for Euler equations with gravity.
- -C. Chalons et al. A large time-step and well-balanced Lagrange-projection type scheme for the shallow-water equations
- -C. Chalons et al. An all-regime Lagrange-projection-like scheme for the gas dynamics equations on unstructured meshes.
- -T. Padioleau et al. A high-performance and portable all-Mach regime flow solver code with well-balanced gravity, application to compressible convection.





Euler's equations for fluid dynamics

 $\begin{cases} \partial_t \rho + \\ \partial_t (\rho u) + \partial_x (u \rho u) \\ \partial_t (\rho E) + \partial_x (u \rho E) \end{cases}$

Desired properties of a numerical method: -> Stability, namely positive preserving and entropy inequality: $\rho > 0, P > 0, and \partial_t \rho s + \partial_r u \rho s \ge 0,$

-> The splitted acoustic/transport solver of Chalons et al. 2016 satisfies all properties !

$$\begin{aligned} \partial_x(\rho u) &= 0, \\ \partial u + P) &= \rho g, \\ E + Pu) &= \rho ug \end{aligned}$$

-> All-regime: The Discretization error has to be independent of the mach number Ma. -> Well-balanced: Preserves the hydrostatic equilibrium $\partial_x P = -\rho \partial_x \phi$, $u_0 = 0$ exactly



The splitted acoustic/transport solver of Chalons et al. 2016

Acoustic system Ac $\partial_t \rho + \rho \partial_x u = 0$ $\partial_t(\rho u) + \rho u \partial_x u + \partial_x p = \rho g$ $\partial_t(\rho E) + \rho E \partial_x u + \partial_x(p u) = \rho u g$

Transport system T $\begin{cases} \partial_t \rho + u \partial_x \rho = 0 \\ \partial_t (\rho u) + u \partial_x (\rho u) = 0 \\ \partial_t (\rho E) + u \partial_x (\rho E) = 0 \end{cases}$

The idea is to resolve both system successively: $U^{n+1} = T(Ac(U^n)) = T(U^{Ac})$:

1) Starting from $(\rho, \rho u, \rho E)^n$, compute $(\rho, \rho u, \rho E)^{Ac}$ by approximating **Ac** 2) Starting from $(\rho, \rho u, \rho E)^{Ac}$, compute $(\rho, \rho u, \rho E)^{n+1}$ by approximating **T**

The splitted acoustic/transport solver of Chalons et al. 2016

reads:

$$\begin{cases} \rho_j^{n+1} = \rho_j^n - \frac{\Delta t}{\Delta x} \left[u^{*,n} \rho \right]^n \\ (\rho u)_j^{n+1} = (\rho u)_j^n - \frac{\Delta t}{\Delta x} \left[u^{*,n} \rho \right]^n \\ (\rho E)_j^{n+1} = (\rho E)_j^n - \frac{\Delta t}{\Delta x} \left[u^{*,n} \rho \right]^n \end{cases}$$

 $\left[Ac \right]_{j\pm 1/2}$

 ${}^{*,n}(\rho u)^{Ac} + \Pi^{*,n}\Big]_{j\pm 1/2} + \Delta t \{\rho g\}_{j}^{n}$ ${}^{*,n}(\rho E)^{Ac} + \Pi u^{*,n}\Big]_{j\pm 1/2} + \Delta t \{\rho u g\}_{j}^{n}$

Our new method:

reads:

$$\begin{cases} \rho_j^{n+1} = \rho_j^n - \frac{\Delta t}{\Delta x} \left[u^{*,n} \rho \right] \\ (\rho u)_j^{n+1} = (\rho u)_j^n - \frac{\Delta t}{\Delta x} \left[u^{*} \right] \\ (\rho E)_j^{n+1} = (\rho E)_j^n - \frac{\Delta t}{\Delta x} \left[u^{*} \right] \end{cases}$$



${}^{*,n}(\rho u)^{n} + \Pi^{*,n}\Big]_{j\pm 1/2} + \Delta t \{\rho g\}_{j}^{n}$ ${}^{*,n}(\rho E)^{n} + \Pi u^{*,n}\Big]_{j\pm 1/2} + \Delta t \{\rho u g\}_{j}^{n}$

Our new method, advantages

reads:

$$\begin{cases} \rho_{j}^{n+1} = \rho_{j}^{n} - \frac{\Delta t}{\Delta x} \left[u^{*,n} \rho^{n} \right]_{j \pm 1/2} \\ (\rho u)_{j}^{n+1} = (\rho u)_{j}^{n} - \frac{\Delta t}{\Delta x} \left[u^{*,n} (\rho u)^{n} + \Pi^{*,n} \right]_{j \pm 1/2} + \Delta t \{ \rho g \}_{j}^{n} \\ (\rho E)_{j}^{n+1} = (\rho E)_{j}^{n} - \frac{\Delta t}{\Delta x} \left[u^{*,n} (\rho E)^{n} + \Pi u^{*,n} \right]_{j \pm 1/2} + \Delta t \{ \rho u g \}_{j}^{n} \end{cases}$$

- Easy to implement (Easy to plug in a flux based finite volume code) -
- -
- -
- Same good properties as the splitted method
- Stencil reduction 2->1
- Half CFL condition (no miracle...)
- operator splitting.

*Intensively studied by Steger & Warming, Zha & Bilgen, Liou & Steffen, Jameson, Bouchut, Toro 14

Easy to combine with a high order algorithm (MUSCL, WENO, MOOD etc...) Memory print is dramatically reduced (no need for an intermediate array) -> HPC

Entirely new kind of mathematical background: Flux splitting method* instead of

- convection ?
- Numerical results
- Why does it works ? -Flux splitting approach-

*Chalons et al. 2016 An all-regime Lagrange-Projection like scheme for the gas dynamics equations on unstructured meshes



Why do we need all-regime well-balanced numerical methods to study

The new solver as a algorithmic simplification of an existing method*

Numerical results, Sod's shock tube (stable)



Numerical results, Atmosphere at rest (Well-Balanced)



17

Numerical results, Rayleigh-Taylor inst. (All-Regime)



Numerical results, Gresho Vortex (All-Regime)



- convection ?
- Numerical results
- Why does it works ? -Flux splitting approach-•

*Chalons et al. 2016 An all-regime Lagrange-Projection like scheme for the gas dynamics equations on unstructured meshes



Why do we need all-regime well-balanced numerical methods to study

The new solver as a algorithmic simplification of an existing method*

Why does it works? -Relaxation and Flux splitting-

Advection system $\partial_t \rho + 2 \partial_x (\rho u) = 0$ $\partial_t(\rho u) + 2\partial_x(u\rho u) = 0$ $\partial_t(\rho E) + 2\partial_x(u\rho E) = 0$ $\partial_t(\rho\Pi) + 2\partial_x(u\rho\Pi) = 0$ $\partial_t(\rho\mathcal{T}) + 2\partial_x(u\rho\mathcal{T}) = 0$

 $\partial_t \rho + \partial_x (\rho u) = 0$ $\partial_t(\rho u) + \partial_y(u\rho u + \Pi) = -\rho \partial_y \phi$ $\partial_t(\rho E) + \partial_x(u\rho E + \Pi u) = -\rho u \partial_x \phi$ $\partial_t(\rho\Pi) + \partial_x\left(u\rho\Pi + a^2u\right) = \rho\lambda(p-\Pi)$ $\partial_t(\rho \mathcal{T}) = 0$

Pressure system



Why does it works? -The averaging interpretation-



Advection step

T JA



$$U_{j}^{n+1} = \frac{U_{j}^{A} + U_{j}^{P}}{2} = \begin{cases} \rho_{j}^{n} - \frac{\Delta t}{\Delta x} \left[u^{*,n} \rho^{n} \right]_{j \pm 1/2} \\ (\rho u)_{j}^{n} - \frac{\Delta t}{\Delta x} \left[u^{*,n} (\rho u)^{n} + \Pi^{*,n} \right]_{j \pm 1/2} + \Delta t \{ \rho g \}_{j}^{n} \\ (\rho E)_{j}^{n} - \frac{\Delta t}{\Delta x} \left[u^{*,n} (\rho E)^{n} + \Pi u^{*,n} \right]_{j \pm 1/2} + \Delta t \{ \rho u g \}_{j}^{n} \end{cases}$$

The update is consistent with the Euler system because of the factor 2 in fluxes of the sub-systems. —>The associated waves are twice as fast. -->In practice, it means that we have to use a CFL number < 0.5

Why does it works ? -time consistency-



Why does it works ? -stability of the Advection flux udpate-

 $\forall b \in \{u, E, \Pi, \mathcal{T}\} \quad (\rho b)_i^A = (\rho b)_i^n - \frac{\Delta t}{\Delta r} \left(u_{i+1/2}^* (\rho b^n)_{i+1/2} - u_{i-1/2}^* (\rho b)_{i-1/2}^n \right),$

 $\leftrightarrow b_i^A = a_1 b_{i+1}^n + a_2 b_i^n + a_3 b_{i-1}^n$

With $a_1 + a_2 + a_3 = 1$ and all $a_i > 0$

Convex combination under CFL condition $\frac{\Delta t}{\Delta x} \left(u_{j+1/2}^{*,+} - u_{j-1/2}^{*,-} \right) < \frac{1}{2}$



Why does it works ? -stability of the Advection flux update-

 $\forall b \in \{u, E, \Pi, \mathcal{T}\}$ $b_j^A = a_1 b_{j+1}^n + a_2 b_j^n + a_3 b_{j-1}^n$ convex combination

Since $(\mathcal{T}, E, u) \to s(\mathcal{T}, e(E, u))$ is concave:

 $(\rho s)_j^A - (\rho s)_j^n + 2 \frac{\Delta t}{\Delta r} \left(u_{j+1}^* \right)$

Entropy inequality for the advection fluxes!

$$u_{1/2}^{*}(\rho s)_{j+1/2}^{n} - u_{j-1/2}^{*}(\rho s)_{j-1/2}^{n} \ge 0 *$$

*Subtlety :
$$(\rho s)_j^A = \rho_j^A s \left(\mathcal{C} \right)_j^A$$



Why does it works ? -stability of the **Pressure** flux update-

Exact same steps as in Chalons et al. 2016 provide:



Where the flux function is consistent with 0, under the pressure CFL condition.

-Result comes from the resolution of the LD Riemann problem for the pressure system -The entropy inequality can be violated for low values of the Low-Mach correction -> Checkerboard modes, not AP

 $(\rho s)_{j}^{P} - (\rho s)_{j}^{n} + 2 \frac{\Delta t}{\Delta r} \left(q_{j+1/2}^{n} - q_{j-1/2}^{n} \right) \ge 0 *$

*Subtlety :
$$(\rho s)_j^P = \rho_j^A s \left(\mathcal{G} \right)_j^P$$



Why does it works ? -stability of the full scheme-

$$(\rho s)_{j}^{A} - (\rho s)_{j}^{n} + 2\frac{\Delta t}{\Delta x} \left(u_{j+1/2}^{*}(\rho s)_{j+1/2}^{n} - u_{j-1/2}^{*}(\rho s)_{j-1/2}^{n} \right) \ge 0$$

 $\rightarrow \frac{(\rho s)_{j}^{P} + (\rho s)_{j}^{A}}{2} - (\rho s)_{j}^{n} + \frac{\Delta t}{\Delta r} \left(u_{j+1/2}^{*} (\rho s)_{j+1/2}^{n} + q_{j+1/2}^{n} - u_{j-1/2}^{*} (\rho s)_{j-1/2}^{n} - q_{j-1/2}^{n} \right) \ge 0$

By concavity of $\eta: (\rho, \rho \mathcal{T}, \rho u, \rho E) \mapsto \rho s$

 $(\rho s)_{j}^{P} - (\rho s)_{j}^{n} + 2 \frac{\Delta t}{\Delta r} \left(q_{j+1/2}^{n} - q_{j-1/2}^{n} \right) \ge 0$

We have $(\rho s)_j^{n+1} > \frac{(\rho s)_j^r + (\rho s)_j^A}{2}$ $\left(\rho \mathcal{T} \left(\rho E\right) \quad (\rho u)^2\right)$

Why does it works ? -stability of the full scheme-

Full entropy inequality:

$$(\rho s)_{j}^{n+1} - (\rho s)_{j}^{n} + \frac{\Delta t}{\Delta x} \left(u_{j+1/2}^{*} (\rho s)_{j+1/2}^{n} + q_{j+1/2}^{n} - u_{j-1/2}^{*} (\rho s)_{j-1/2}^{n} - q_{j-1/2}^{n} \right) \ge 0$$

Is indeed a discrete equivalent of:

 $\partial_t \rho s + \partial_x u \rho s \ge 0.$

Conclusion-perspectives

- The procedure was also applied successfully to splitted Lagrange-projection methods for other systems; -Ideal MHD, M1 model for radiative transfer. Should also work for shallowwater equations and the 5 equations two phases flow model.
- The flux-based update we obtained was successfully plugged in existing MUSCL and MOOD based codes,
- Implicit/explicit approach for the low Mach CFL issue should be straightforward,
- One important issue remains: The checkerboard modes.
- Main takeaway: If you use a splitted method, give the un-splitting a shot !

Thanks for your attention

Why does it works ? -stability of the advection step-

 $\forall b \in \{u, E, \Pi, \mathcal{T}\} \quad (\rho b)_i^A = (\rho b)_i^n -$

$$\leftrightarrow \left(\frac{\rho b}{\rho}\right)_{j}^{A} = \lambda_{j}^{(+1)} \left(\frac{\rho b}{\rho}\right)_{j+1}^{n} + \lambda_{j}^{(0)} \left(\frac{\rho b}{\rho}\right)_{j}^{n} + \lambda_{j}^{(-1)} \left(\frac{\rho b}{\rho}\right)_{j-1}^{n}$$

Where
$$\lambda_{j}^{(+1)} = -\frac{\Delta t}{\Delta x} u_{j+1/2}^{*,-} \left(\frac{\rho_{j+1}^{n}}{\rho_{j}^{A}} \right), \quad \lambda_{j}^{(0)} = \left[1 - \frac{\Delta t}{\Delta x} \left(u_{j+1/2}^{*,+} - u_{j-1/2}^{*,-} \right) \right] \left(\frac{\rho_{j}^{n}}{\rho_{j}^{A}} \right), \quad \lambda_{j}^{(-1)} = \frac{\Delta t}{\Delta x} u_{j-1/2}^{*,+} \left(\frac{\rho_{j}^{n}}{\rho_{j}^{A}} \right), \quad \lambda_{j}^{(-1)} = \frac{\Delta t}{\Delta x} u_{j-1/2}^{*,+} \left(\frac{\rho_{j}^{n}}{\rho_{j}^{A}} \right), \quad \lambda_{j}^{(-1)} = \frac{\Delta t}{\Delta x} u_{j-1/2}^{*,+} \left(\frac{\rho_{j}^{n}}{\rho_{j}^{A}} \right), \quad \lambda_{j}^{(-1)} = \frac{\Delta t}{\Delta x} u_{j-1/2}^{*,+} \left(\frac{\rho_{j}^{n}}{\rho_{j}^{A}} \right), \quad \lambda_{j}^{(-1)} = \frac{\Delta t}{\Delta x} u_{j-1/2}^{*,+} \left(\frac{\rho_{j}^{n}}{\rho_{j}^{A}} \right), \quad \lambda_{j}^{(-1)} = \frac{\Delta t}{\Delta x} u_{j-1/2}^{*,+} \left(\frac{\rho_{j}^{n}}{\rho_{j}^{A}} \right), \quad \lambda_{j}^{(-1)} = \frac{\Delta t}{\Delta x} u_{j-1/2}^{*,+} \left(\frac{\rho_{j}^{n}}{\rho_{j}^{A}} \right), \quad \lambda_{j}^{(-1)} = \frac{\Delta t}{\Delta x} u_{j-1/2}^{*,+} \left(\frac{\rho_{j}^{n}}{\rho_{j}^{A}} \right),$$

Since $\rho_{j}^{A} = -\frac{\Delta t}{\Delta x} u_{j+1/2}^{*,-} \rho_{j+1}^{n} + \frac{\Delta t}{\Delta x} u_{j-1/2}^{*,+} \rho_{j-1}^{n} +$

 $\lambda_{j}^{(+1)} + \lambda_{j}^{(0)} + \lambda_{j}^{(-1)} = 1 : \text{convex combination under CFL condition} \quad \frac{\Delta t}{\Delta x} \left(u_{j+1/2}^{*,+} - u_{j-1/2}^{*,-} \right) < 1 !$

$$\frac{\Delta t}{\Delta x} \left(u_{i+1/2}^* (\rho b^n)_{i+1/2} - u_{i-1/2}^* (\rho b)_{i-1/2}^n \right),$$

+
$$\left[1 - \frac{\Delta t}{\Delta x} \left(u_{j+1/2}^{*,+} - u_{j-1/2}^{*,-}\right)\right] \rho_j^n$$
, we have

31



Why does it works ? -stability of the advection step- simplifier

$$\forall b \in \{u, E, \Pi, \tau\}, \left(\frac{\rho b}{\rho}\right)_j^A = \lambda_j^{(+1)} \left(\frac{\rho b}{\rho}\right)_{j+1}^n + \lambda_j^{(0)} \left(\frac{\rho b}{\rho}\right)_j^n + \lambda_j^{(-1)} \left(\frac{\rho b}{\rho}\right)_{j-1}^n, \lambda_j^{(+1)} + \lambda_j^{(0)} + \lambda_j^{(-1)} + \lambda_j^{(-1$$

Noting $e(u, E) = E - \frac{1}{2}u^2$, we have that: e

$$e_j^A > e_{j+1}^n \lambda_j^{(+1)} + e_j^n \lambda_j^{(0)} + e_{j-1}^n \lambda_j^{(-1)}$$
 by conca

Since $(\mathcal{T}, E, u) \to s(\mathcal{T}, e(E, u))$ is concave too:

 $\rho_j^A s\left(\mathcal{T}_j^A, e_j^A\right) - \rho_j^n s_j^n + \frac{\Delta t}{\Delta x} \left(u_{j+1/2}^* \rho_{j+1/2}^n s_{j+1/2}^n - u_{j-1/2}^* \rho_{j-1/2}^n s_{j-1/2}^n\right) \ge 0$



Why does it works ? -stability of the Pressure step-

Exact same steps as in Chalons et al. 2016 provide:

 $\rho_j^P s\left(\mathcal{T}_j^P, e_j^P\right) - \rho_j^n s\left(1/\rho_j^n, e_j^n\right) + \frac{\Delta t}{\Delta r}\left(q_{j+1/2}^n - q_{j-1/2}^n\right) \ge 0$

Where the flux function is consistent with 0, under the pressure CFL condition.

-Result comes from the resolution of the LD Riemann problem for the pressure system -The entropy inequality can be violated for low values of the Low-Mach correction -> Checkerboard modes, not AP



Why does it works ? -stability of the full scheme- simplifier

 $\rho_j^P s\left(\mathcal{T}_j^P, e_j^P\right) - \rho_j^n s\left(1/\rho_j^n, e_j^n\right) + \frac{\Delta t}{\Delta r} \left(q_{j+1/2}^n - q_{j-1/2}^n\right) \ge 0$

 $\rightarrow \frac{\rho_{j}^{P} s\left(\mathcal{T}_{j}^{P}, e_{j}^{P}\right) + \rho_{j}^{A} s\left(\mathcal{T}^{A}, e_{j}^{A}\right)}{2} - \rho_{j}^{n} s\left(1/\rho_{j}^{n}, e_{j}^{n}\right) + \frac{\Delta t}{2\Delta x} \left(u_{j+1/2}^{*} \rho_{j+1/2}^{n} s_{j+1/2}^{n} - u_{j-1/2}^{*} \rho_{j-1/2}^{n} s_{j-1/2}^{n} - q_{j-1/2}^{n}\right) \geq 0$

 $\rho_j^A s\left(\mathcal{T}_j^A, e_j^A\right) - \rho_j^n s_j^n + \frac{\Delta t}{\Delta x_i} \left(u_{j+1/2}^* \rho_{j+1/2}^n s_{j+1/2}^n - u_{j-1/2}^* \rho_{j-1/2}^n s_{j-1/2}^n\right) \ge 0$

We need $\rho_j^{n+1} s(1/\rho_j^{n+1}, e_j^{n+1}) > \frac{\rho_j^P s\left(\mathcal{T}_j^P, e_j^P\right) + \rho_j^A s\left(\mathcal{T}_j^A, e_j^A\right)}{2}$



$$\begin{split} \text{We need } \rho_{j}^{n+1}s(1/\rho_{j}^{n+1},e_{j}^{n+1}) > \frac{\rho_{j}^{P}s\left(\mathcal{T}_{j}^{P},e_{j}^{P}\right) + \rho_{j}^{A}s\left(\mathcal{T}_{j}^{A},e_{j}^{A}\right)}{2} \\ \text{We define } \eta:(\rho,\rho\mathcal{T},\rho u,\rho E) \mapsto \rho s\left(\frac{\rho\mathcal{T}}{\rho},\frac{(\rho E)}{\rho}-\frac{(\rho u)^{2}}{2\rho^{2}}\right) \\ \rho_{j}^{n+1}s\left(1/\rho_{j}^{n+1},e_{j}^{n+1}\right) = \rho_{j}^{n+1}s\left(\frac{1}{\rho_{j}^{n+1}},\frac{(\rho E)_{j}^{n+1}}{\rho_{j}^{n+1}}-\frac{1}{2}\left(\frac{(\rho u)_{j}^{n+1}}{\rho_{j}^{n+1}}\right)^{2}\right) = \eta\left(\rho_{j}^{n+1},1,(\rho u)_{j}^{n+1},(\rho E)_{j}^{n+1}\right) \\ = \eta\left(\rho_{j}^{n+1},(\rho\mathcal{T})_{j}^{n+1},(\rho u)_{j}^{n+1},(\rho E)_{j}^{n+1}\right) = \eta\left(\sum_{k=A,P}\frac{\rho_{j}^{k}}{2},\sum_{k=A,P}\frac{(\rho\mathcal{T})_{j}^{k}}{2},\sum_{k=A,P}\frac{(\rho u)_{j}^{k}}{2},\sum_{k=A,P}\frac{(\rho E)_{j}^{k}}{2}\right). \end{split}$$

$$\begin{split} \text{We need } \rho_{j}^{n+1} s(1/\rho_{j}^{n+1}, e_{j}^{n+1}) > & \frac{\rho_{j}^{P} s\left(\mathcal{T}_{j}^{P}, e_{j}^{P}\right) + \rho_{j}^{A} s\left(\mathcal{T}_{j}^{A}, e_{j}^{A}\right)}{2} \\ \text{We define } \eta : (\rho, \rho \mathcal{T}, \rho u, \rho E) \mapsto \rho s\left(\frac{\rho \mathcal{T}}{\rho}, \frac{(\rho E)}{\rho} - \frac{(\rho u)^{2}}{2\rho^{2}}\right) \\ s^{n+1} s\left(1/\rho_{j}^{n+1}, e_{j}^{n+1}\right) = \rho_{j}^{n+1} s\left(\frac{1}{\rho_{j}^{n+1}}, \frac{(\rho E)_{j}^{n+1}}{\rho_{j}^{n+1}} - \frac{1}{2}\left(\frac{(\rho u)_{j}^{n+1}}{\rho_{j}^{n+1}}\right)^{2}\right) = \eta\left(\rho_{j}^{n+1}, 1, (\rho u)_{j}^{n+1}, (\rho E)_{j}^{n+1}\right) \\ = \eta\left(\rho_{j}^{n+1}, (\rho \mathcal{T})_{j}^{n+1}, (\rho u)_{j}^{n+1}, (\rho E)_{j}^{n+1}\right) = \eta\left(\sum_{k=A,P} \frac{\rho_{j}^{k}}{2}, \sum_{k=A,P} \frac{(\rho \mathcal{T})_{j}^{k}}{2}, \sum_{k=A,P} \frac{(\rho u)_{j}^{k}}{2}, \sum_{k=A,P} \frac{(\rho E)_{j}^{k}}{2}\right). \end{split}$$

Lemma: η is concave, thus:

$$\rho_j^{n+1}s\left(1/\rho_j^{n+1}, e_j^{n+1}\right) \ge \sum_{k=A,P} \frac{1}{2}\eta\left(\rho_j^k, (\rho\mathcal{T})_j^k, (\rho u)_j^k, (\rho E)_j^k\right) = \sum_{k=A,P} \frac{1}{2}\rho_j^k s\left(\mathcal{T}_j^k, e_j^k\right)$$

Why does it works ? -stability of the full scheme- simplifier