

University-industry collaboration : Modeling and simulation for gas distribution.

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1 - INTRODUCTION

1.1 - SUMMIT (SORBONNE UNIVERSITÉ MAISON DES MODÉLISATIONS, INGÉNIERIES ET TECHNOLOGIES)

- ▶ Our university:  SORBONNE UNIVERSITÉ
- ▶ Our services: provide high-quality engineering research to private and public partners.
- ▶ Our expertise:
 - ▶ Modeling Simulation and Optimization.
 - ▶ Data science, IA.
 - ▶ Hybrid modeling.
- ▶ Some projects:
 - ▶ Obepine - Genome quantification in wastewaters / development of smoother / model reduction of compartmental models etc.
 - ▶ Eau de Paris - anomaly detection / classification / calibration etc.
 - ▶ **GTT - Low Mach model for gas transport.**

1 - INTRODUCTION

1.2 - History of a collaboration for gas transport with GTT.



1 - INTRODUCTION

1.3 - Issue

1. Complete compressible Navier-Stokes Equation:

$$\frac{\partial \rho}{\partial t} + \operatorname{div}(\rho \mathbf{u}) = 0$$

$$\frac{\partial \rho \mathbf{u}}{\partial t} + \operatorname{div}(\rho \mathbf{u} \otimes \mathbf{u}) + \nabla P = \rho \mathbf{g} + \operatorname{div}(\boldsymbol{\sigma})$$

+ State Equation
+ Temperature Equation

$$(\mathbf{u} \otimes \mathbf{w} = \mathbf{u} \mathbf{w}^T)$$

2. Compressible: good representation of the physical phenomena but not applicable in practice (CFL condition too restrictive in the low Mach number regime)
3. Incompressible: not enough to obtain a good representation
4. **Proposition: build a quasi-incompressible model:**

▶ Good physical representation + Applicable numerical scheme

2 - Objective

2.1 - A quasi-incompressible model

- ▶ Obtain a model of the form:

$$\operatorname{div}(\mathbf{u}) = A(T, P)P'(t) + B(T, P)\operatorname{div}(q_T), \quad (1)$$

$$\rho D_t \mathbf{u} = -\nabla \Pi + \frac{1}{Re} \operatorname{div}(\boldsymbol{\sigma}) - \frac{\rho}{Fr}, \quad (2)$$

$$C_p D_t T = \left(-\frac{T}{\rho} \frac{\partial \rho}{\partial T} \Big|_P \right) P'(t) - \frac{1}{Re Pr} \operatorname{div}(q_T), \quad (3)$$

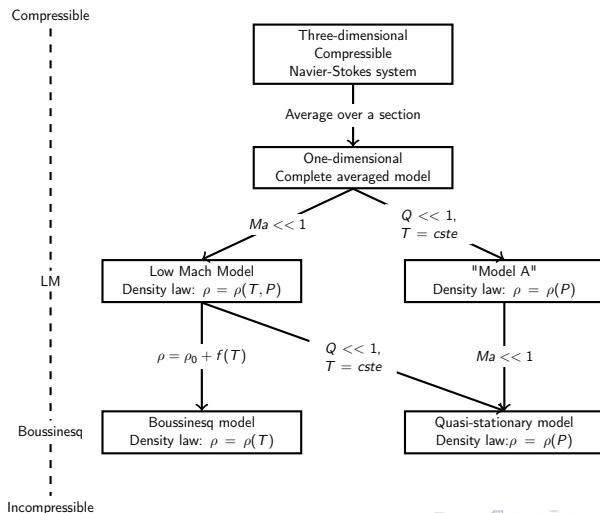
$$\rho = \rho(T, P), \quad (4)$$

with

- ▶ Π : the dynamic pressure
- ▶ P : the thermodynamic pressure
- ▶ Equation (1) : the quasi-incompressibility constraint
- ▶ Equation (4) : equation of state

2 - Objective

2.1 - A quasi-incompressible model



3 - Modeling

3.1 - 1D Averaged Navier-Stokes equations for ideal gases

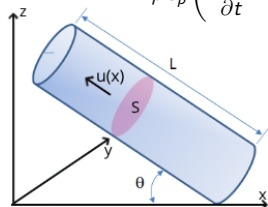
1D AVERAGED NAVIER-STOKES EQUATIONS for ideal gases

$$\frac{\partial S\rho}{\partial t} + \frac{\partial S\rho u}{\partial x} = 0,$$

$$\frac{\partial S\rho u}{\partial t} + \frac{\partial S\rho u^2}{\partial x} + \frac{\partial SP}{\partial x} = -\tau\pi D - \rho Sg \sin \theta,$$

$$\rho C_p \left(\frac{\partial ST}{\partial t} + u \frac{\partial ST}{\partial x} \right) = D_t(SP) + u\tau\pi D - 2\pi Rq_w,$$

$$\rho = \frac{P}{rT}.$$



3 - Modeling

3.2 - Derivation

- ▶ Characteristic values L_c, U_c, t_c such that $L_c = U_c t_c$
- ▶ Dimensionless variables $\tilde{x} = \frac{x}{L_c}, \tilde{t} = \frac{t}{t_c}, \tilde{u} = \frac{u}{U_c}, \tilde{\rho} = \frac{\rho}{\rho_c}$

$$\frac{\partial \tilde{S} \tilde{\rho}}{\partial \tilde{t}} + \frac{\partial \tilde{S} \tilde{\rho} \tilde{u}}{\partial \tilde{x}} = 0,$$

$$\frac{\partial \tilde{S} \tilde{\rho} \tilde{u}}{\partial \tilde{t}} + \frac{\partial \tilde{S} \tilde{\rho} \tilde{u}^2}{\partial \tilde{x}} + \frac{1}{\gamma Ma^2} \frac{\partial \tilde{S} \tilde{P}}{\partial \tilde{x}} = -\frac{f}{2} \pi \tilde{\rho} \tilde{u}^2 \tilde{D} - \frac{1}{Fr} \tilde{S} \tilde{\rho} g \sin \theta,$$

$$\tilde{C}_p \tilde{\rho} \left(\frac{\partial \tilde{S} \tilde{T}}{\partial \tilde{t}} + \tilde{u} \frac{\partial \tilde{S} \tilde{T}}{\partial \tilde{x}} \right) = \frac{\gamma - 1}{\gamma} D_{\tilde{t}}(\tilde{S} \tilde{P}) + (\gamma - 1) Ma^2 \frac{f}{2} \pi \tilde{\rho} \tilde{u}^3 \tilde{D} - \frac{2\pi \tilde{R}}{Pr Re} \tilde{q}_w.$$

$$Ma^2 = \frac{\rho_c u_c^2}{\gamma P_c}$$

$$Fr = \frac{u_c^2}{L_c g}$$

$$Re = \frac{u_c L_c \rho_c}{\mu_c}$$

$$Pr = \frac{\mu_c C_{pc}}{k_c}$$

3 - Modeling

3.2 - Derivation

Asymptotic development:

$$\begin{aligned}\tilde{u}(x, t) &= \tilde{u}_0(x, t) + Ma\tilde{u}_1(x, t) + \mathcal{O}(Ma^2), \\ \tilde{P}(x, t) &= \tilde{P}_0(x, t) + Ma\tilde{P}_1(x, t) + Ma^2\Pi(x, t) + \mathcal{O}(Ma^3).\end{aligned}$$

$$\begin{aligned}\frac{\partial \tilde{S}\tilde{\rho}_0}{\partial \tilde{t}} + \frac{\partial \tilde{S}\tilde{\rho}_0\tilde{u}_0}{\partial \tilde{x}} &= 0, \\ \frac{\partial \tilde{S}\tilde{\rho}_0\tilde{u}_0}{\partial \tilde{t}} + \frac{\partial \tilde{S}\tilde{\rho}_0\tilde{u}_0^2}{\partial \tilde{x}} + \frac{1}{\gamma} \frac{\partial \tilde{S}\Pi}{\partial \tilde{x}} &= -\frac{f}{2}\pi\tilde{\rho}_0\tilde{u}_0^2\tilde{D} - \frac{1}{Fr}\tilde{\rho}_0\tilde{S}g\sin\theta, \\ \tilde{\rho}_0\tilde{C}_p \left(\frac{\partial \tilde{S}\tilde{T}_0}{\partial \tilde{t}} + \tilde{u}_0 \frac{\partial \tilde{S}\tilde{T}_0}{\partial \tilde{x}} \right) &= \frac{\gamma-1}{\gamma}\tilde{S}\tilde{P}'_0 - \frac{2\pi\tilde{R}}{PrRe}\tilde{q}_w.\end{aligned}$$

3 - Modeling

3.2 - Derivation

$$\frac{\partial Su}{\partial x} = -\frac{S}{\gamma P} P'(t) - \frac{2\pi R(\gamma - 1)}{\gamma P} q_w, \quad (6)$$

$$\partial_t u + u \partial_x u + \frac{\partial_x \Pi}{\rho} = -\frac{f}{2} \pi u^2 \frac{D}{S} - g \sin \theta, \quad (7)$$

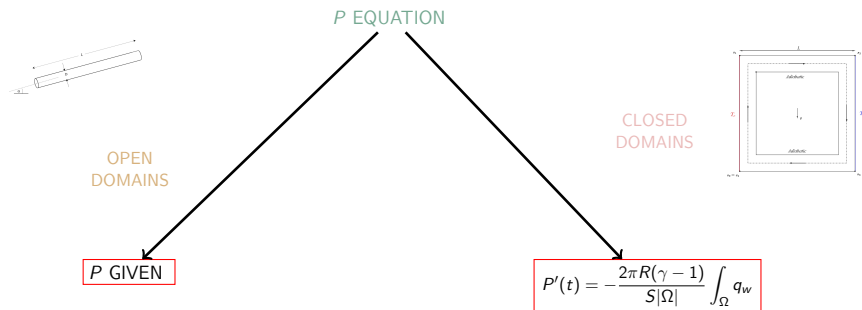
$$\rho C_p \left(\frac{\partial ST}{\partial t} + u \frac{\partial ST}{\partial x} \right) = S P'(t) - 2\pi R q_w. \quad (8)$$

We will denote

$$\eta = \frac{\partial Su}{\partial x}$$

3 - Modeling

3.3 - Boundary conditions



4 - Numerical Method

4.1 - Equation for T

Method of characteristics

$$\left(\frac{\partial T}{\partial t} + u \frac{\partial T}{\partial x} \right) = f(x, t) = \frac{(\gamma - 1)T(x, t)}{\gamma P(t)} P'(t) - \frac{2\pi R(\gamma - 1)T(x, t)}{S\gamma P(t)} q_w$$



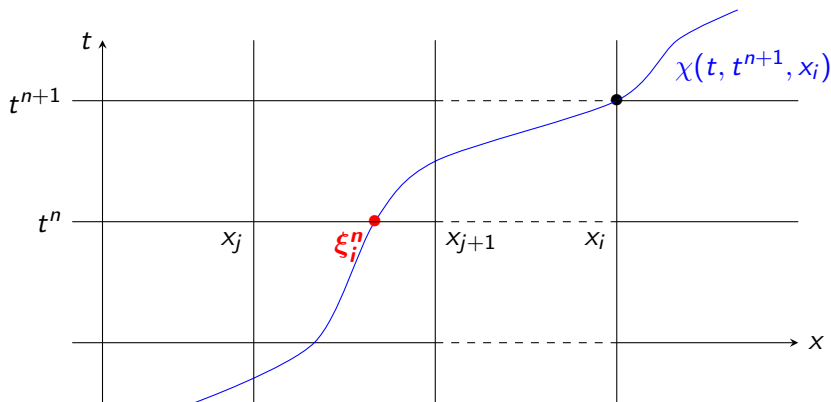
$$T_i^{n+1} = \hat{T}_i^n + \Delta t f(T_i^{n+1}, P^n, \rho^n)$$



$$T_i^{n+1} = \frac{\hat{T}_i^n + \Delta t \left(\frac{(\gamma-1)T_i^n}{\gamma P(t^n)} P'(t^n) + \frac{2\pi R(\gamma-1)T_i^n h}{\gamma S P(t^n)} T_{ref} \right)}{1 + \Delta t \frac{2\pi R(\gamma-1)T_i^n h}{\gamma S P(t^n)}}$$

4 - Numerical Method

4.2 - Method of characteristics



4 - Numerical Method

4.3 - Equation for Π

Equation for Π and u :

- ▶ Elliptic equation for Π :

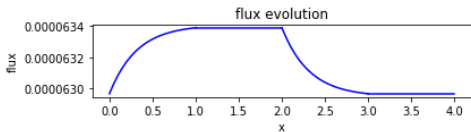
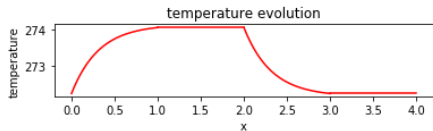
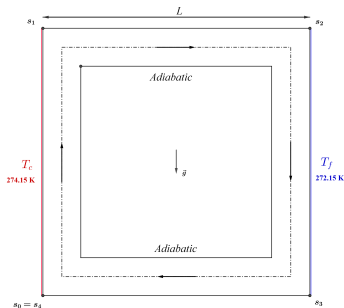
$$-\partial_x \left(\frac{\partial_x \Pi}{\rho} \right) = \partial_t \eta + u \partial_x \eta + \eta^2 + f \pi u \eta \frac{D}{S} - g \delta(x - nL).$$

- ▶ Method of characteristics for u :

$$u_i^{n+1} = \frac{\hat{u}_i^n + \Delta t \left(-\frac{rT_i^{n+1}}{P(t^{n+1})} \frac{\Pi_i^{n+1} - \Pi_{i-1}^{n+1}}{\Delta x} - g \sin \theta \right)}{1 + \Delta t \frac{f}{S} \pi D}$$

5 - Pseudo analytical solution

5.1 - Periodic case



5 - Pseudo analytical solution

5.1 - Periodic case

$$\frac{\partial Su}{\partial x} = -\frac{S}{\gamma P} P'(t) - \frac{2\pi R(\gamma - 1)}{\gamma P} q_w,$$

$$\partial_t u + u \partial_x u + \frac{\partial_x \Pi}{\rho} = -\frac{f}{2} \pi u^2 \frac{D}{S} - g \sin \theta,$$

$$\rho C_p \left(\frac{\partial ST}{\partial t} + u \frac{\partial ST}{\partial x} \right) = SP'(t) - 2\pi R q_w.$$

5 - Pseudo analytical solution

5.1 - Periodic case

$$T(x) = T_{ref} + (T_0 - T_{ref})e^{-\frac{2\pi R(\gamma-1)h}{\gamma P\Gamma}x}.$$

$$Q(x) = \Gamma T(x).$$

$$\Pi(x) = \frac{bP\Gamma}{rBhT_{ref}}(\ln T(x) - \ln T_0) + \frac{P}{rT_{ref}}(aT_{ref}\Gamma - b)x + \Pi_0.$$

Where:

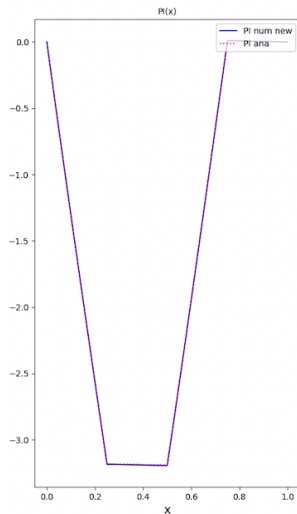
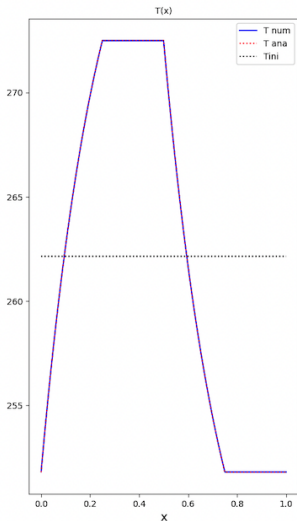
$$\Gamma := \frac{Q_0}{T_0} = \frac{Q_1}{T_1}.$$

$$f(\Gamma) = 0.$$

- └ Pseudo analytical solution
 - └ Numerical results - analytical solution

5 - Pseudo analytical solution

5.2 - Numerical results - analytical solution

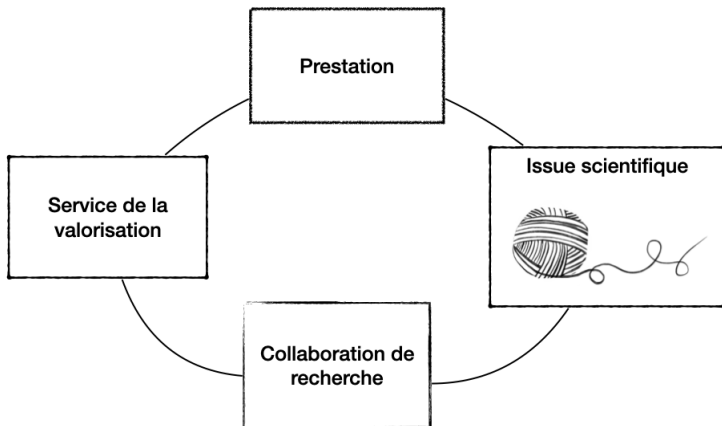


6 - Conclusion

- ▶ We have developed a one dimensional low Mach model.
- ▶ We provided a set of analytical solutions.
- ▶ We have given a validation of the thermosiphon solution.

6 - Conclusion

6.1 - A long-term research collaboration



Thank you !

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